



Free Vibration of Annular Plates by Discrete Singular Convolution and Differential Quadrature Methods

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Abstract

Plates and shells are significant structural components in many engineering and industrial applications. In this study, the free vibration analysis of annular plates is investigated. To this aim, two different numerical methods including the differential quadrature and the discrete singular convolution methods are performed for numerical simulations. Moreover, the Frequency values are obtained via these two methods and finally, the performance of these methods is investigated.

Keywords: Differential quadrature; Discrete singular convolution; Annular plate; Free vibration.

1. Introduction

There are several applications for circular and annular plates in civil, aerospace, petroleum, nuclear, and mechanical engineering. They are used as aircraft fuselages, rockets and turbo jets, reactor walls, ship and submarine parts, holding tanks, etc. This paper deals with the application of the Discrete Singular Convolution (DSC) and the Differential Quadrature (DQ) methods for the free vibration analysis of thin annular plates with clamped and simply supported boundary conditions. The solutions of plate and shell problems have been an interesting issue for engineers and researchers since past 100 years. Therefore, different analytical and numerical methods have been used for this analysis [1-9]. This study focused on DSC and DQ methods.

2. Discrete singular convolution (DSC)

Consider a distribution, T , and $\eta(t)$ as an element of the space of the test function. A singular convolution can be defined as follows [10-15] :

$$F(t) = (T * \eta)(t) = \int_{-\infty}^{\infty} T(t-x)\eta(x)dx, \quad (1)$$

where $T(t-x)$ is a singular kernel. The mathematical property or requirement of $f(x)$ is determined by the approximate kernel T_α . The Shannon's kernel is regularized as follows [16-28]:

$$\delta_{\Delta,\sigma}(x-x_k) = \frac{\sin[(\pi/\Delta)(x-x_k)]}{(\pi/\Delta)(x-x_k)} \exp\left[-\frac{(x-x_k)^2}{2\sigma^2}\right]; \sigma > 0. \quad (2)$$

where Δ is the grid spacing. In the DSC method, the function $f(x)$ and its derivatives with respect to the x coordinate at a grid point x_i are approximated by a linear sum of discrete values $f(x_k)$. This can be expressed as follows [29-46]:

$$\left. \frac{d^n f(x)}{dx^n} \right|_{x=x_i} = f^{(n)}(x) \approx \sum_{k=-M}^M \delta_{\Delta,\sigma}^{(n)}(x_i-x_k) f(x_k); \quad (n=0, 1, 2, \dots). \quad (3)$$

where superscript n denotes the n th-order derivative with respect to x .

3. Differential Quadrature Method (DQM)

Similar to the other numerical analysis techniques, such as the finite element or finite difference methods, the DQM also transforms the given differential equation into a set of analogous algebraic equations in terms of the unknown function values at the resampled points in the domain. The problem areas, in which the applications of differential quadrature method may be found in the available literature, include static and dynamic structural mechanics and the stability analysis of structures [47-55]. Recently, the DQM has been largely developed by Bert et al. [53] who were the first to suggest the method as a tool for the structural analysis. In fact, they had made most of effective supplements to the theory and application of the DQM. Mainly on the vibration analysis of plates, the recent works of Bert et al. [53] have contributed significantly to the development of the DQM [52, 53].

It has been claimed that the DQM has the capability of producing highly accurate solutions with minimal computational effort. All this work has demonstrated that the application of the DQ methods leads to accurate results with less computational effort and there is a potential that the method may become an alternative to the conventional methods such as finite differences and finite elements. Therefore, research on the extension and application of the method becomes an important endeavor. In the differential quadrature method, a partial derivative of a function with respect to a space variable at a discrete point is approximated as a weighted linear sum of the function values at all discrete points in the region of that variable. For simplicity, a one-dimensional function $\psi(x)$ in the $[-1, 1]$ domain and N discrete points are considered. Then, the first derivatives at point i as $x = x_i$ is given as follows: [53]

$$\Psi_x(x_i) = \left. \frac{\partial \Psi}{\partial x} \right|_{x=x_i} = \sum_{j=1}^N A_{ij} \Psi(x_j); \quad i = 1, 2, \dots, N \quad (4)$$

where x_j are the discrete points in the variable domain, $\psi(x_j)$ are the function values at these points and A_{ij} are the weighting coefficients for the first order derivative attached to these function values. Two methods have been suggested to determine the weighting coefficients. The first one is to let Eq. (1) be exact for the test functions as

$$\psi_k(x) = x^{k-1}, \quad k = 1, 2, \dots, N \quad (5)$$

which leads to a set of linear algebraic equations as

$$(k-1)x_i^{k-2} = \sum_{j=1}^N A_{ij} x_j^{k-1}; \quad \text{for } i = 1, 2, \dots, N \quad \text{and} \quad k = 1, 2, \dots, N \quad (6)$$

which represents N sets of N linear algebraic equations. This equation system has a unique solution because its matrix is a Vandermonde matrix. Regarding the weighting coefficients, this equation may be solved analytically by using the Hamming's method [51-54] or the numerical method which applies certain special algorithms for Vandermonde equations, such as the methods proposed by Bjorck and Pereyra [47-54]. Similar to the first order, the second order derivative can be written as

$$\Psi_{xx}(x_i) = \frac{\partial^2 \Psi}{\partial x^2} \Big|_{x=x_i} = \sum_{j=1}^N B_{ij} \Psi(x_j); \quad i = 1, 2, \dots, N \tag{7}$$

where the B_{ij} is the weighting coefficients for the second order derivative. Equation (4) also can be written as

$$\Psi_{xx}(x_i) = \frac{\partial^2 \Psi}{\partial x^2} \Big|_{x=x_i} = \sum_{j=1}^N A_{ij} \sum_{k=1}^N A_{jk} \Psi(x_k); \quad i = 1, 2, \dots, N \tag{8}$$

4. Free vibration analysis of annular plate

The governing equation for a thin and isotropic circular/annular plate (Fig.1) under the axisymmetric motion is given as

$$\frac{\partial^4 u}{\partial r^4} + \frac{2}{r} \left(\frac{\partial^3 u}{\partial r^3} \right) - \frac{1}{r^2} \left(\frac{\partial^2 u}{\partial r^2} \right) + \frac{1}{r^3} \left(\frac{\partial u}{\partial r} \right) + \frac{\rho h}{D} \left(\frac{\partial^2 u}{\partial t^2} \right) = 0 \tag{9}$$

For the free vibration, the transverse displacement u is assumed as

$$u(r,t) = U(R) e^{i\omega t} \tag{10}$$

Substituting the above-mentioned equation into equation (4) and its normalizing yields

$$\frac{\partial^4 U}{\partial R^4} + \frac{2}{R} \left(\frac{\partial^3 U}{\partial R^3} \right) - \frac{1}{R^2} \left(\frac{\partial^2 U}{\partial R^2} \right) + \frac{1}{R^3} \left(\frac{\partial U}{\partial R} \right) - \Omega^2 U = 0 \tag{11}$$

where $R = r/a$, a is the outside radius of the plate, h is the thickness of the plate, D is the flexural rigidity, and Ω is the dimensionless frequency and given $\Omega^2 = \rho h \omega^2 a^4 / D$. Equation (11) can be written by applying the DSC as

$$\sum_{k=-M}^M \delta_{\Delta,\sigma}^{(4)}(k\Delta x) U_{k,j} + \frac{2}{R_i} \sum_{k=-M}^M \delta_{\Delta,\sigma}^{(3)}(k\Delta x) U_{k,j} - \frac{1}{R_i^2} \sum_{k=-M}^M \delta_{\Delta,\sigma}^{(2)}(k\Delta x) U_{k,j} + \frac{1}{R_i^3} \sum_{k=-M}^M \delta_{\Delta,\sigma}^{(1)}(k\Delta x) U_{k,j} = \Omega^2 U_{k,j} \tag{12}$$

The boundary and regularity conditions can be written in a similar way. Consequently, the remaining eigenvalue problem is solved to obtain the natural frequencies. Equation (11) can be easily written in DQ form as

$$\sum_{k=-M}^M D_{ij} U_{k,j} + \frac{2}{R_i} \sum_{k=-M}^M \delta_{\Delta,\sigma}^{(3)} C_{ij} U_{k,j} - \frac{1}{R_i^2} \sum_{k=-M}^M B_{ij} U_{k,j} + \frac{1}{R_i^3} \sum_{k=-M}^M A_{ij} U_{k,j} = \Omega^2 U_{k,j} \tag{13}$$

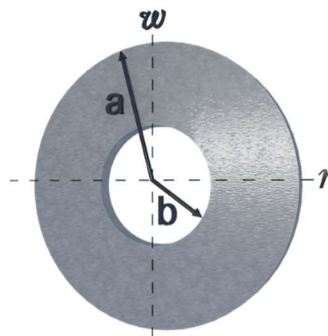


Fig.1. A typical annular plate

5. Results and discussions

The following combination of boundary conditions have been considered while both inner and outer edges are clamped (C-C). Table 1 summarizes the numerical results of first three frequencies by using DSC for the clamped circular plates. By using the generalized differential quadrature (GDQ) method, the first three frequencies obtained by Du et al. [54] are also presented in Table 1. It is apparent that the results were analyzed very well through analytical [7] and GDQ solutions [54]. As can be seen in Table 1, the obtained natural frequencies found by DSC and DQ are very accurate.

The obtained results of the annular plate are presented in Table 2 for the different radius ratios of b/a and S-S type edges. Table 2 presents the non-dimensional fundamental frequencies for the annular plates. In this table, a is the inner radius and b is the outer radius of annular plates. It is observed that a good agreement exists between DQ and DSC results.

Table 1. First three frequencies of the C-C circular plates

Natural frequencies	DQ N=17 This study	GDQ (Ref.54)	Exact (Ref.7)	DSC (N=17) This study
Ω_1	10.21	10.20	10.22	10.23
Ω_2	39.77	44.68	39.77	40.01
Ω_3	89.10	80.24	89.10	89.11

Table 2. Non-dimensional fundamental frequency of the S-S annular plate

b/a	DQ (N=17)	DSC (N=17)	DSC (N=19)	DQ (N=19)
0.1	14.54	14.56	14.56	14.56
0.2	16.83	16.85	16.85	16.85
0.3	21.10	21.11	21.11	21.11
0.4	28.15	28.17	28.17	28.17
0.5	40.09	40.11	40.11	40.11

6. Conclusion

In the present study, the free vibration analysis of thin circular plates and annular plates has been briefly discussed. The approach has been validated through the comparison with convergence studies and existing results in the literature. It is found that the convergence of DSC and DQ methods are very good and the results agree well with those obtained by other researchers. For higher modes (after the 20th modes), which has not been presented here, the method of DSC gives good results than DQ.

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